

Time-resolved investigation of the exhaust emissions of upgrading units

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Partners:



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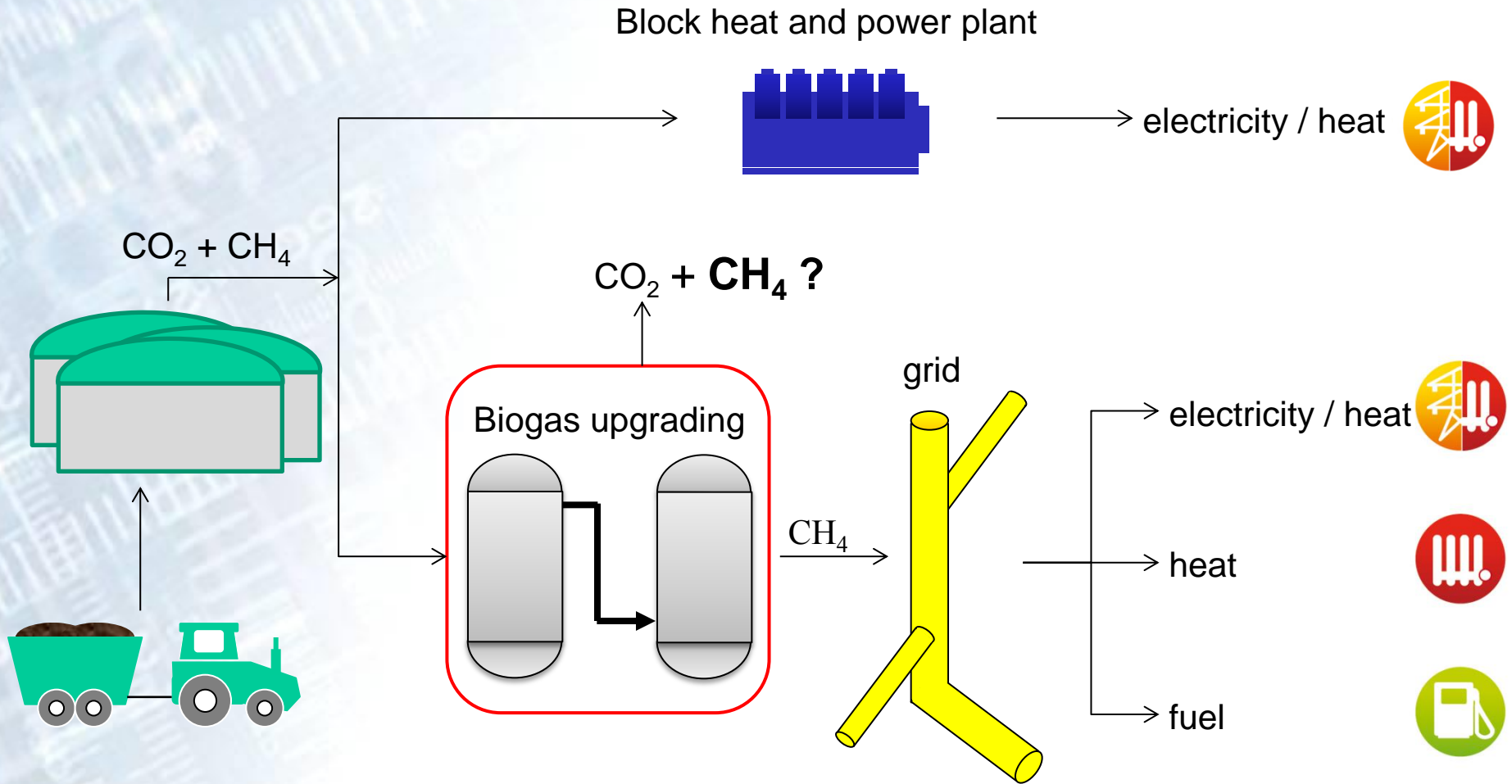


based on a decision of the Parliament
of the Federal Republic of Germany

Investigation of methane losses during the caloric upgrading of biogas for grid injection

- Introduction
- Biogas upgrading technologies
- Determination of methane loss
- Measuring equipment
- Investigation of the characteristics of the flow metering unit
- Practical experience
- Conclusion

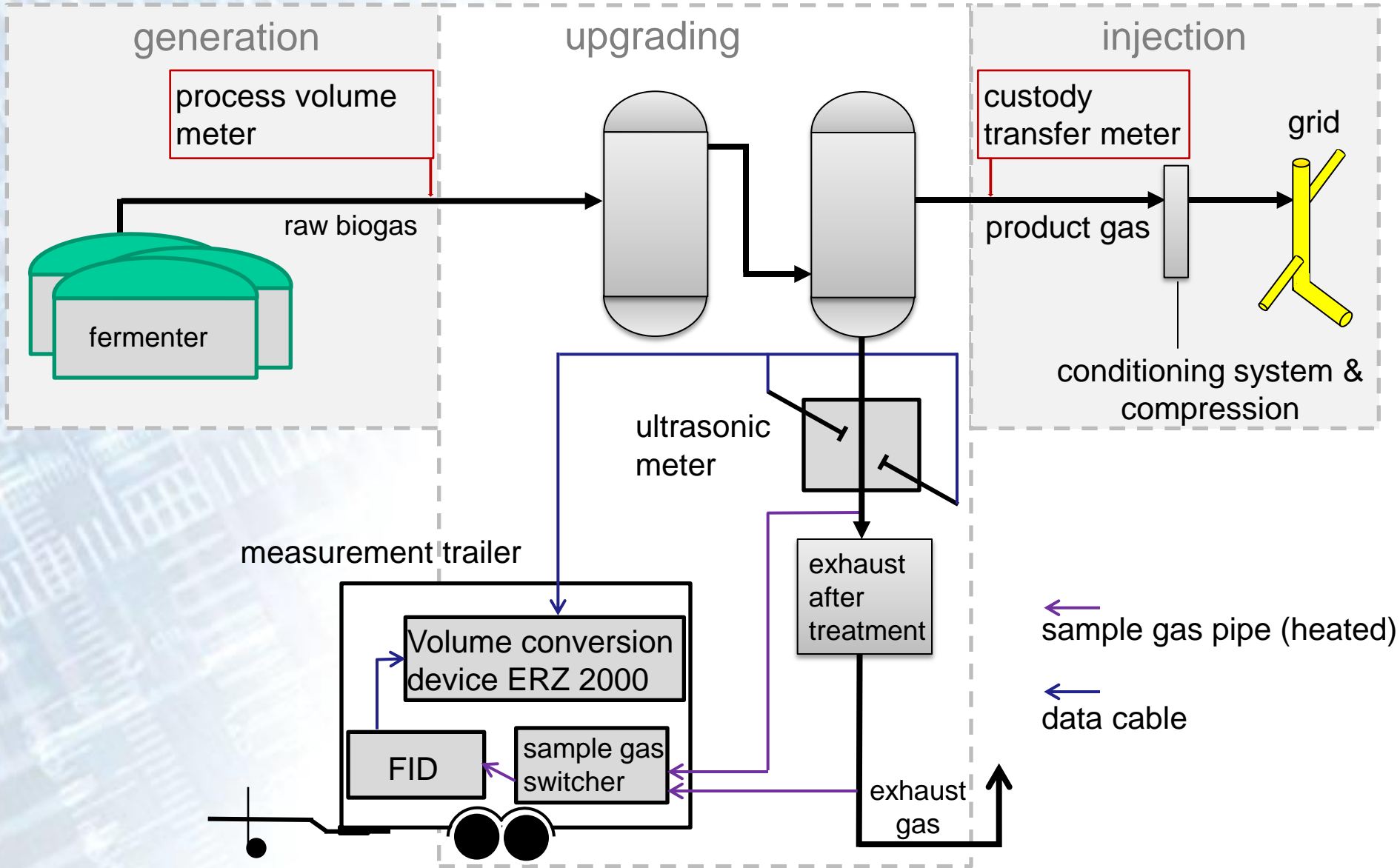
Introduction



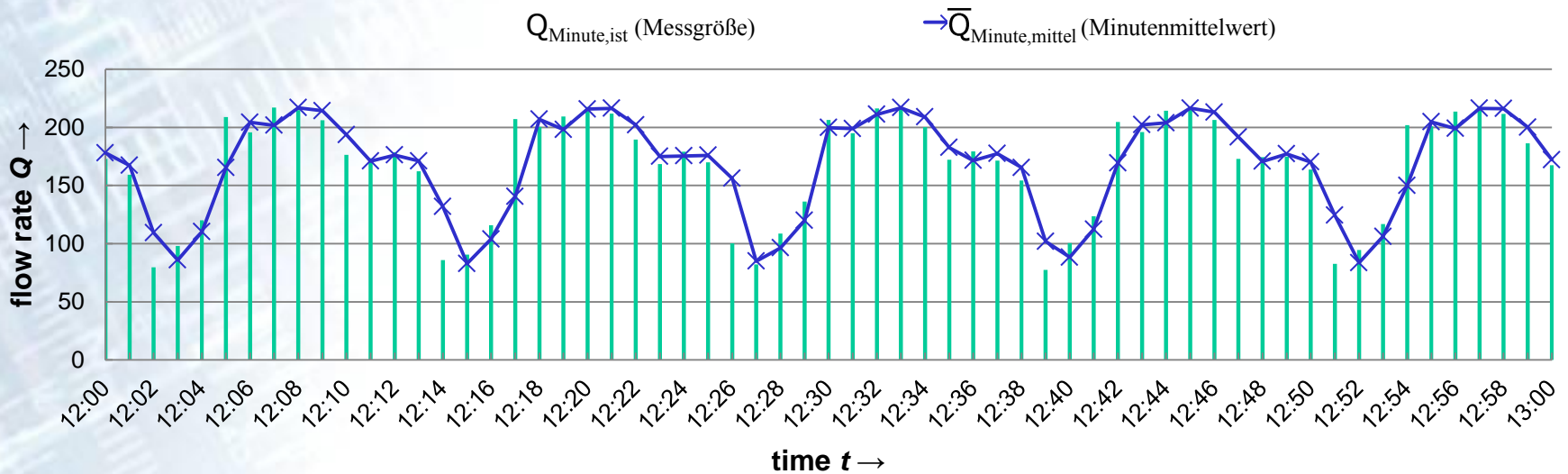
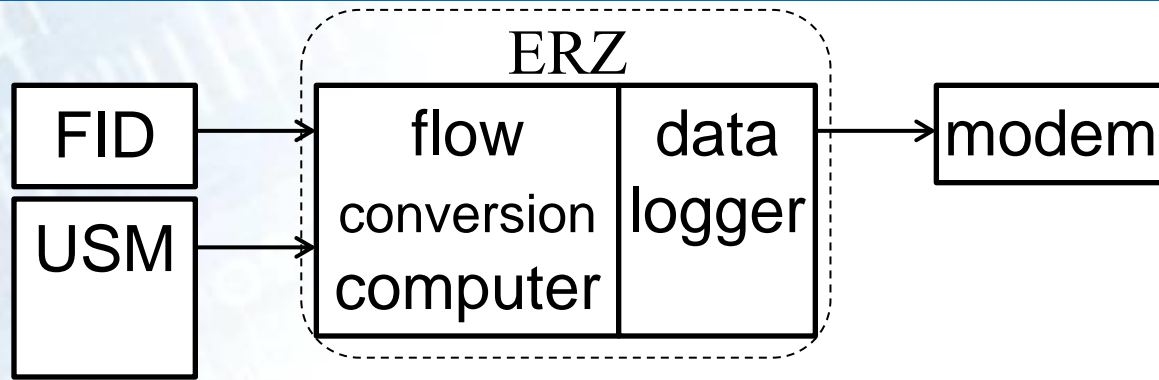
Biogas upgrading technologies

- Steps for the upgrading process
 - desulphurization
 - drying
 - extraction of other contaminates
 - the order of steps depends on the upgrading technique
 - **CO₂ extraction**
- common upgrade techniques
 - pressure swing adsorption
 - water scrubbing
 - chemical scrubbing
 - membrane technologies

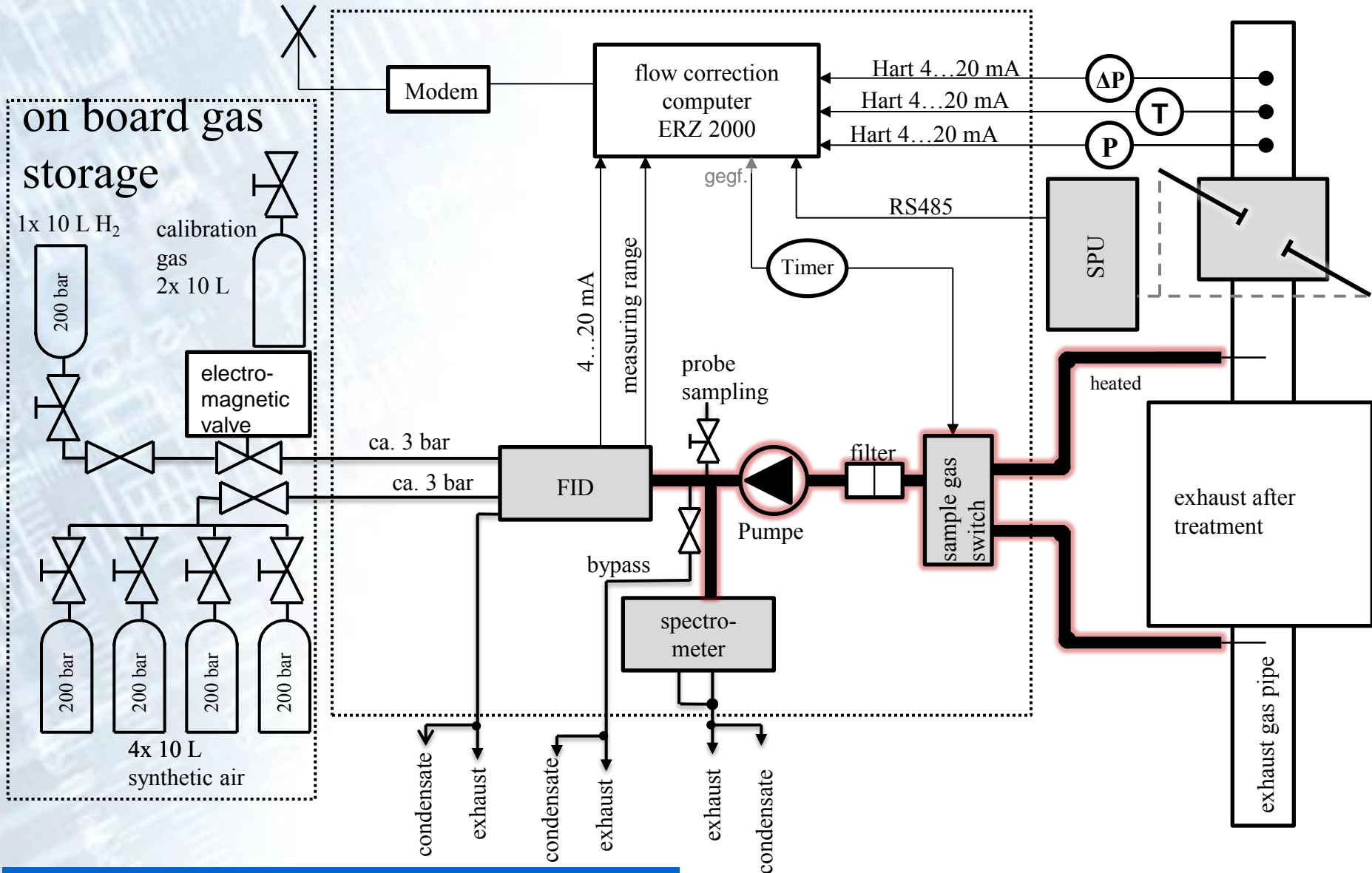
Determination of methane loss



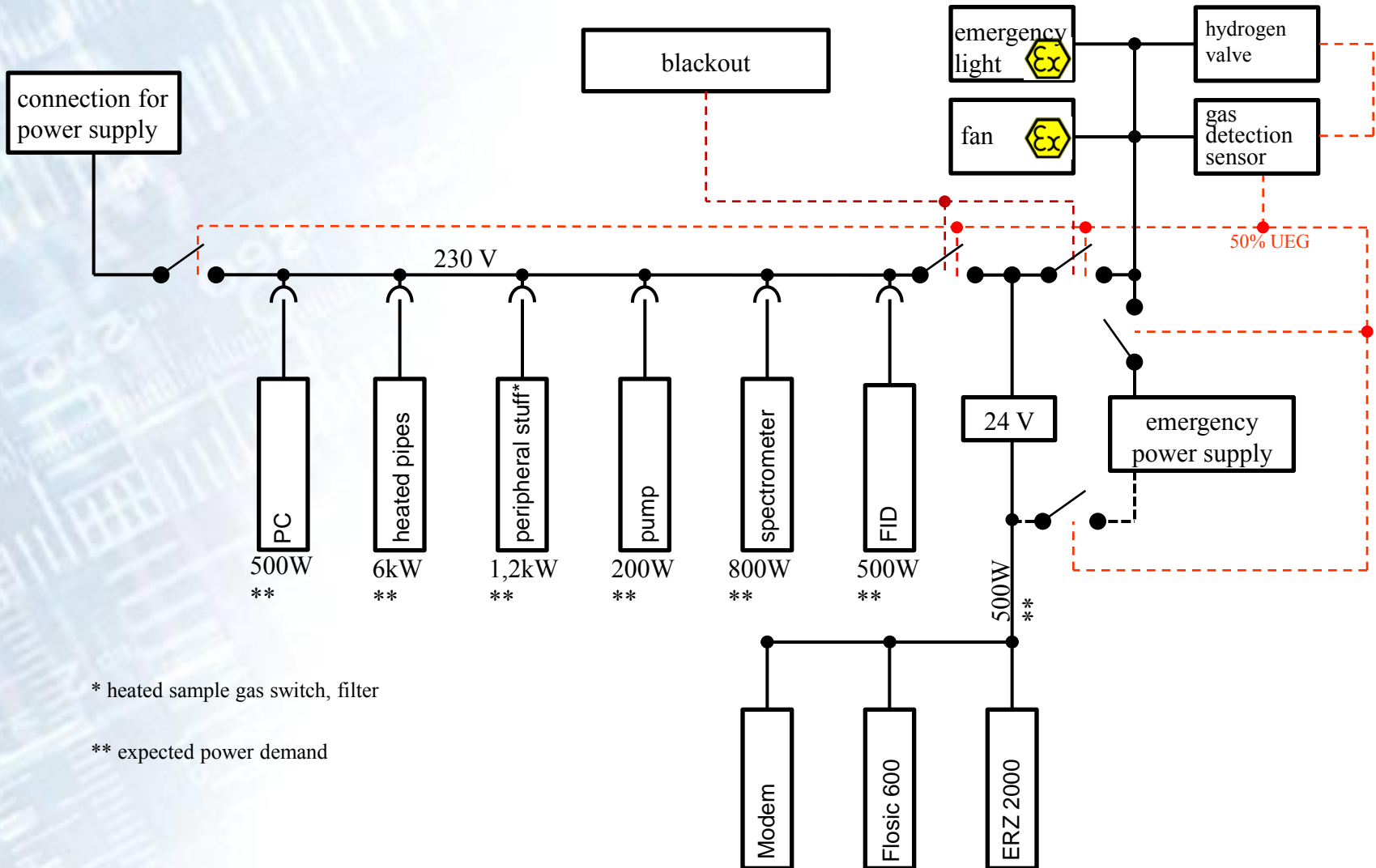
Determination of methane loss



Measuring equipment



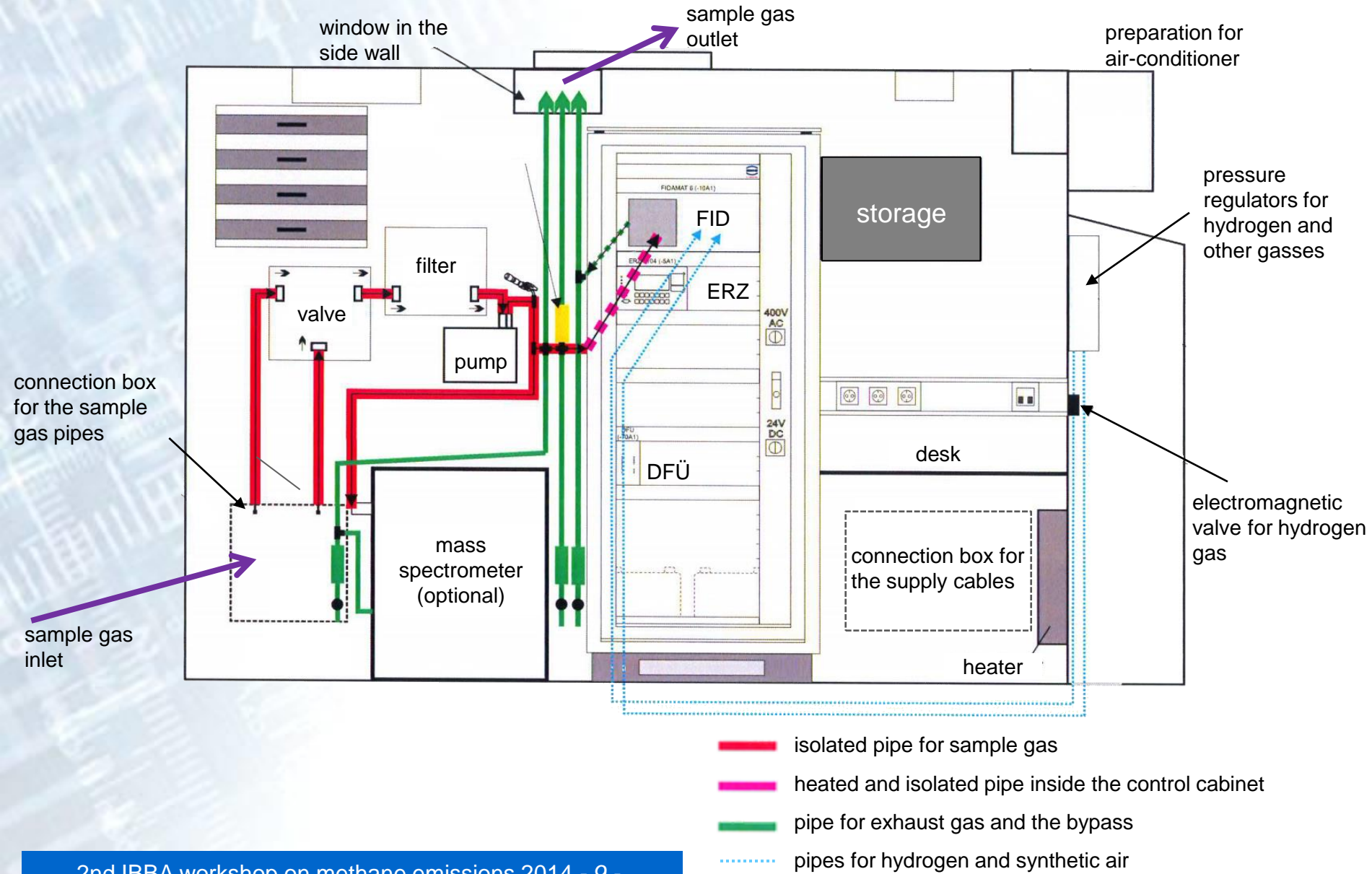
Measuring equipment



* heated sample gas switch, filter

** expected power demand

Measuring equipment



- █ isolated pipe for sample gas
- █ heated and isolated pipe inside the control cabinet
- █ pipe for exhaust gas and the bypass
- █ pipes for hydrogen and synthetic air

Measuring equipment



Measuring equipment



Measuring equipment



Measuring equipment



Measuring equipment

- methane measurement
 - flame ionisation detector (FID)
 - in presence of up to 100 % H₂O vapor
 - calibration with 0.1 to 5 Vol.-% methane in nitrogen
 - calibration with 0.15 to 3 Vol.-% methane in carbon dioxide
- Methan Emissionen

$$E_{CH_4} = Q_{Abgas} \cdot x_{V,CH_4}$$

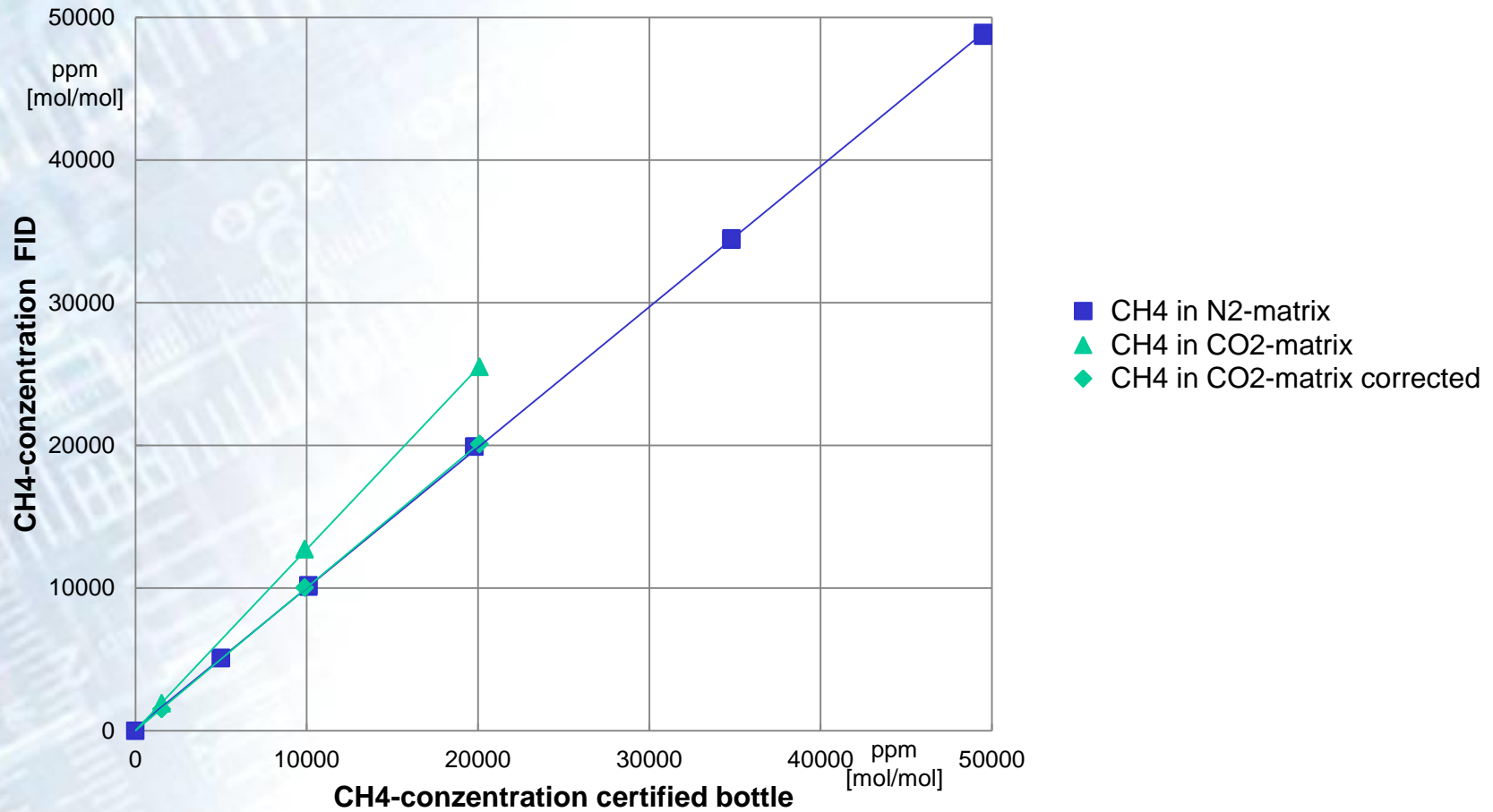
$$x_{V,CH_4} = \frac{x_{CH_4} \cdot \frac{\tilde{M}_{CH_4}}{\rho_{n,CH_4}}}{\sum_{i=1}^k x_i \cdot \frac{\tilde{M}_i}{\rho_{n,i}}}$$



Quelle: Siemens

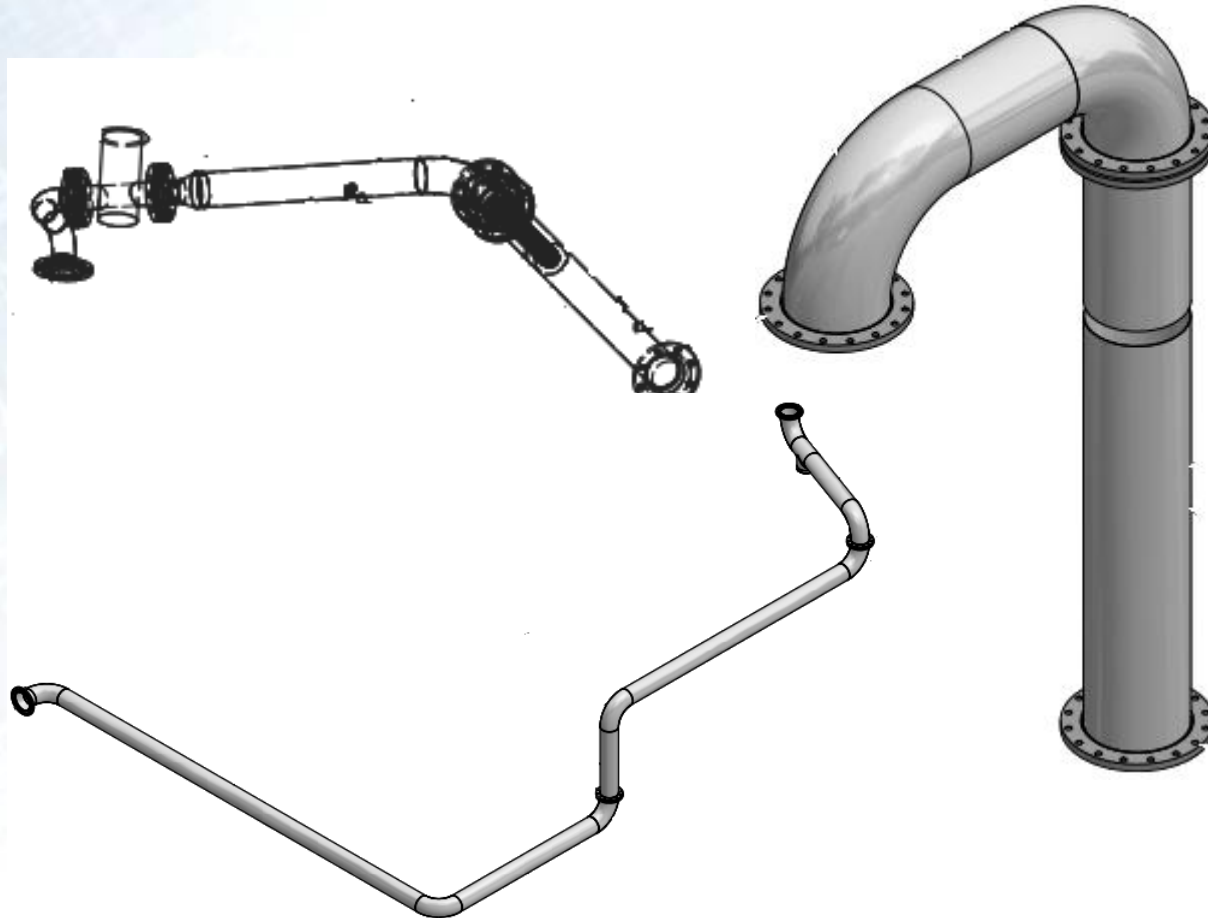


Deviation of FID



Measuring equipment

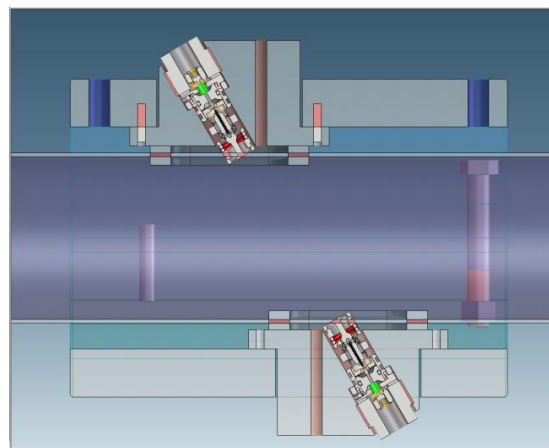
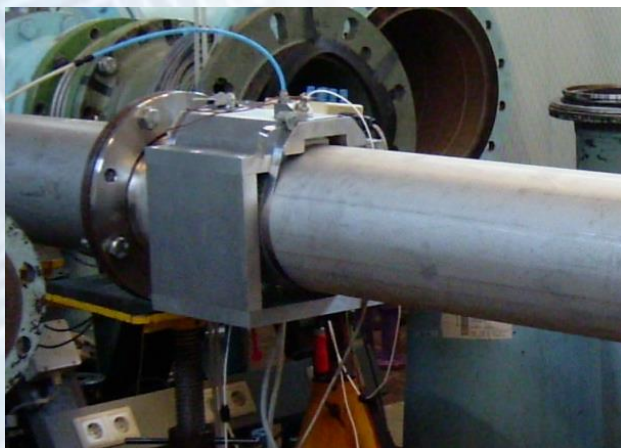
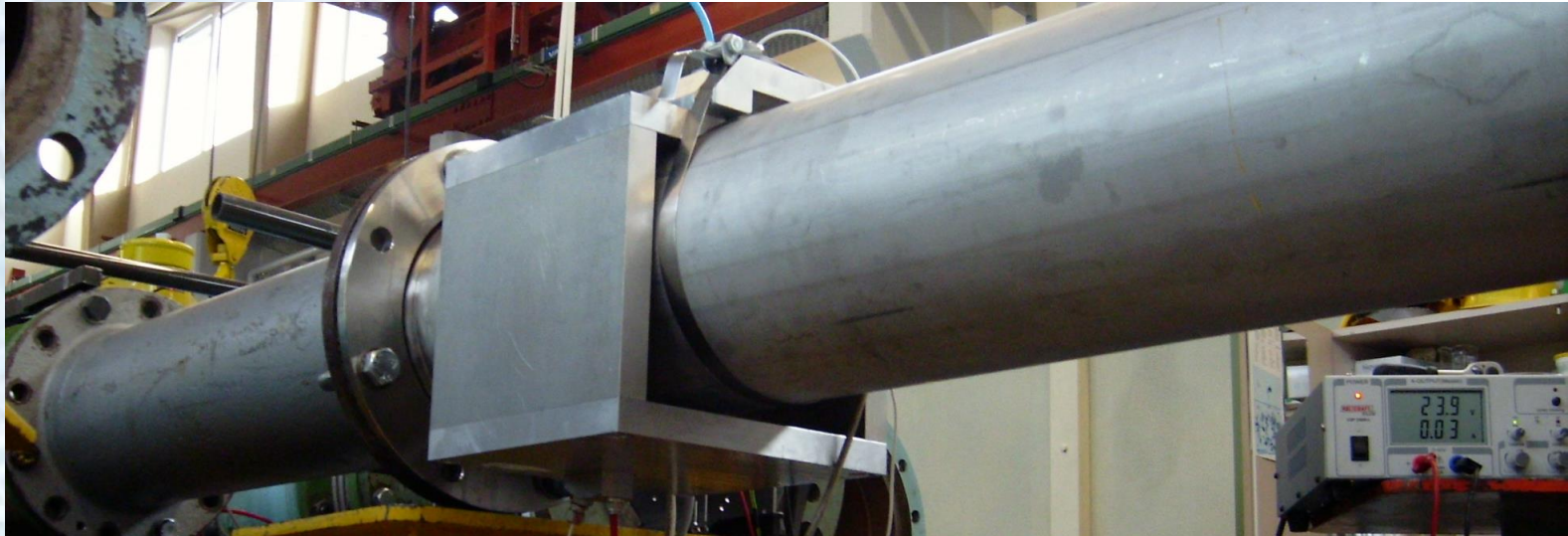
pipeline route: exhaust gas



Flow measuring technique

technique	advantage	disadvantage
commercial available meter	<ul style="list-style-type: none"> high measurement accuracy low perturbation sensitivity (type-dependent) 	<ul style="list-style-type: none"> flanges are needed big interference in local structure high installation effort
ultrasonic measuring probe	<ul style="list-style-type: none"> low interference in local structure (only one drilled whole necessary) speed of sound is available 	<ul style="list-style-type: none"> only parts of the flow profile are measurable adjustment of the correct angle is difficult due to probe size a limited work capability in respect to pipe diameter is possible $\geq \text{DN}100$
ultrasonic meter clamp-on-technique	<ul style="list-style-type: none"> no interference in local structure speed of sound is available sensors can be used for different pipe diameters 	<ul style="list-style-type: none"> fluid pressure has to be high enough signal damping by CO_2 is problematic temperature and pressure measurement needs tape
one-path-ultrasonic meter with sleeve	<ul style="list-style-type: none"> low interference in local structure (two drills) sensors can be used in connection with different sleeves for different pipe diameters speed of sound is available 	<ul style="list-style-type: none"> relatively high perturbation sensitivity
differential pressure (with Prandtl/ Pitot -probe)	<ul style="list-style-type: none"> low interference in local structure (only one drilled whole is necessary) 	<ul style="list-style-type: none"> very high perturbation sensitivity density of gas has to be determined

Measuring equipment

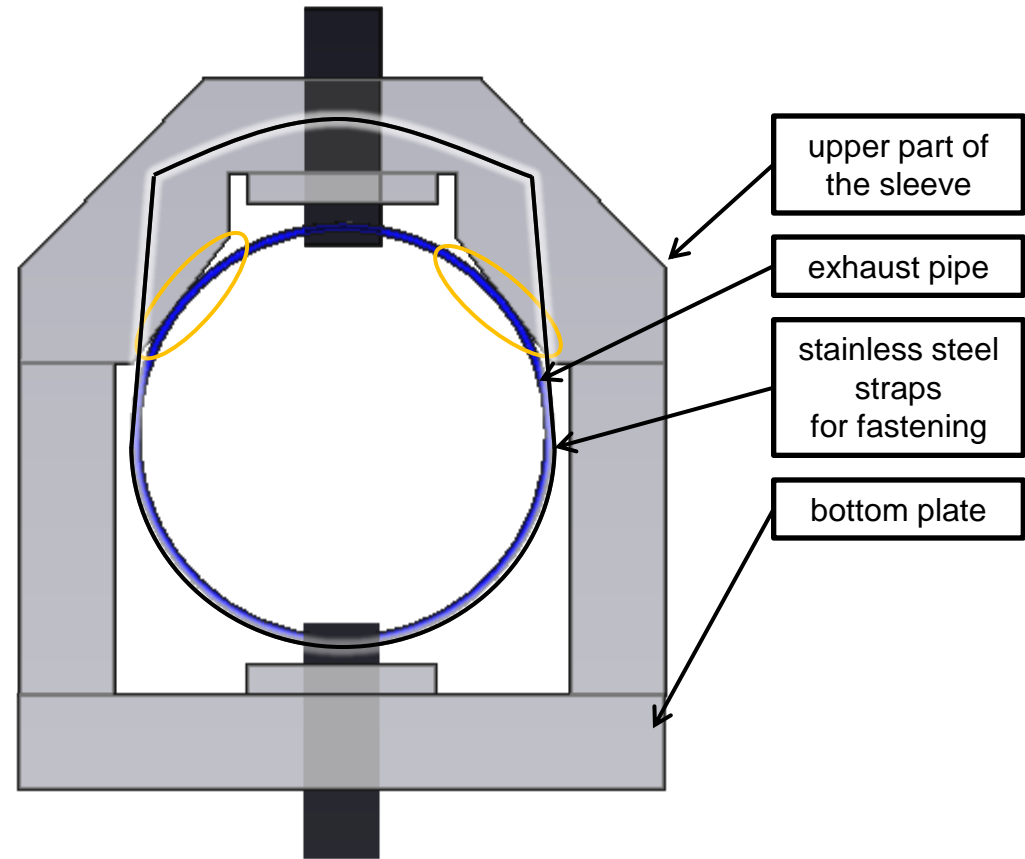
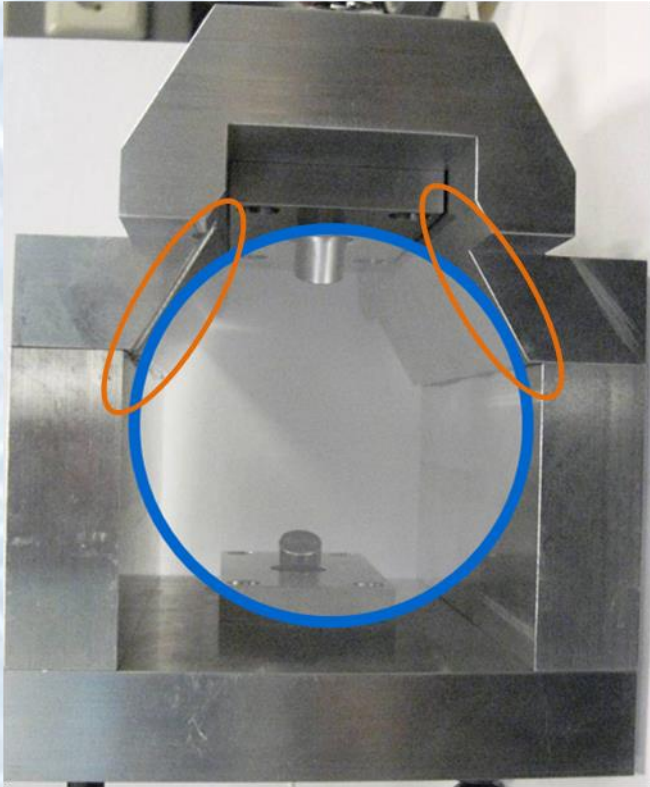


Quelle: SICK

sleeve sizes:

- DN 80
- DN 200
- DN 300

Measuring equipment



Measuring equipment

- flowmeasurement

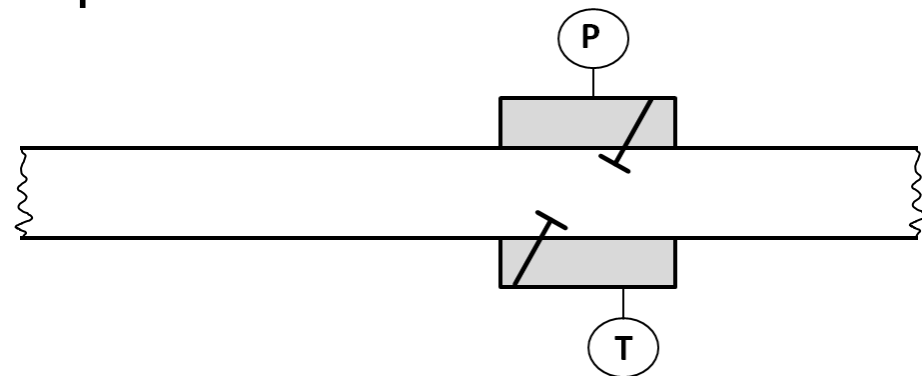
$$Q_V^* = \bar{v} \cdot \frac{D_i^2 \cdot \pi}{4}$$

$$Q_V = Q_V^* \cdot (1 + k(Q_V^*))$$

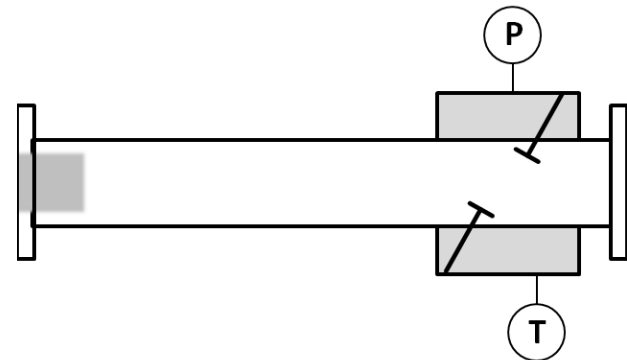
$$k(Q_V^*) = 0$$

- uncorrected

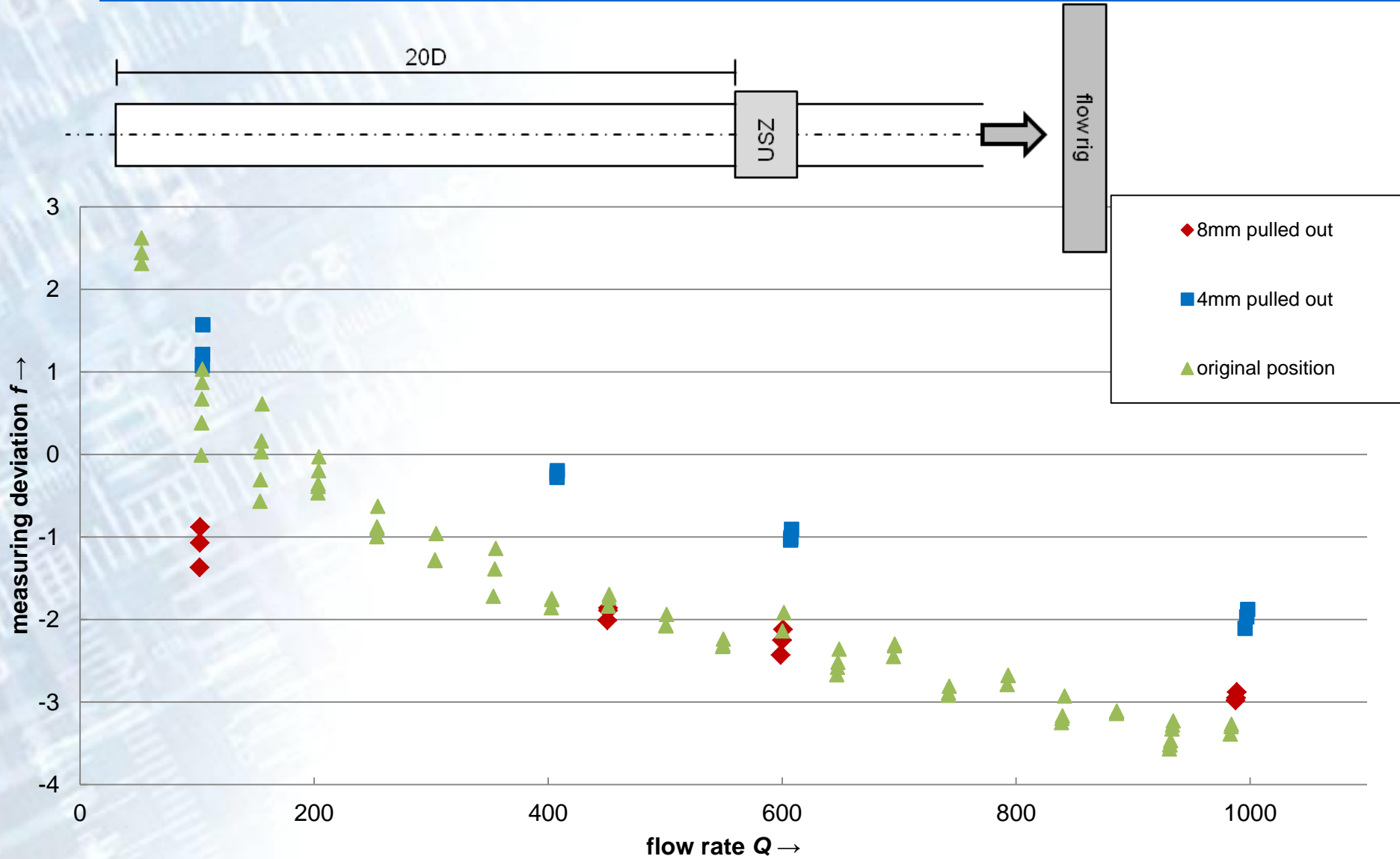
Option 1



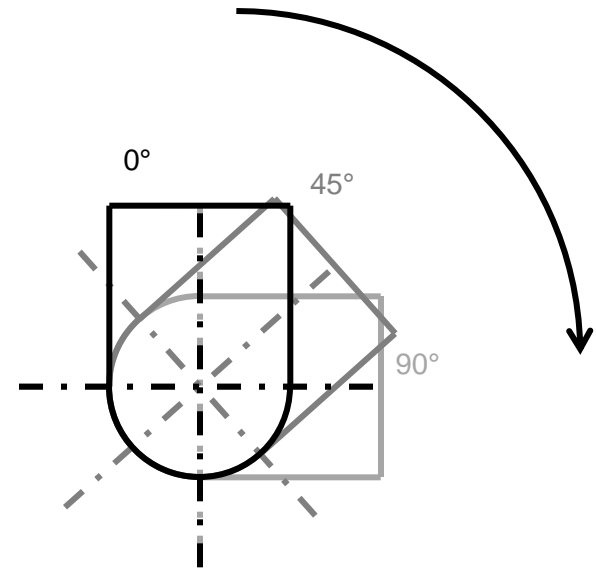
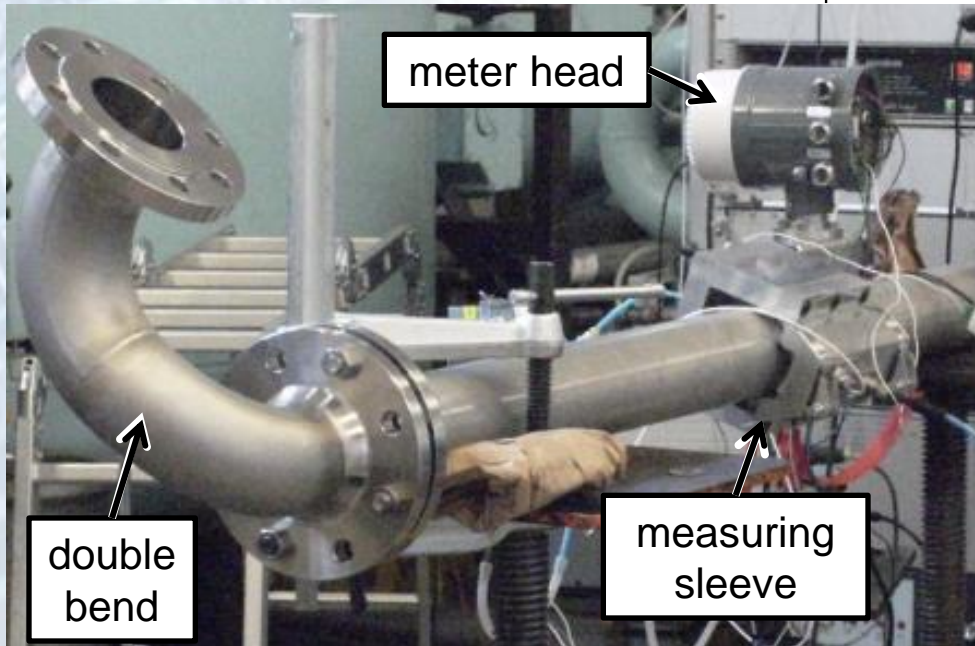
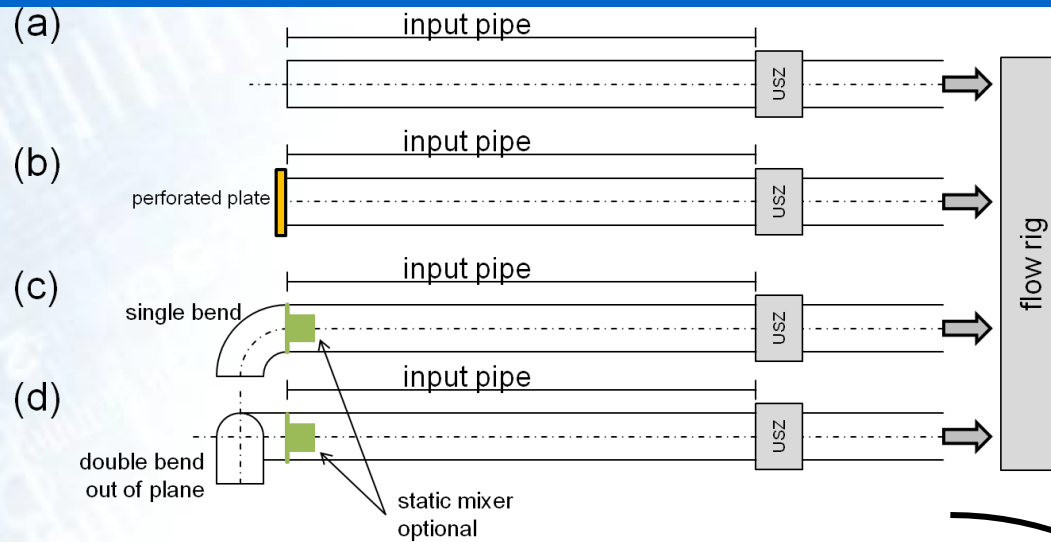
Option 2



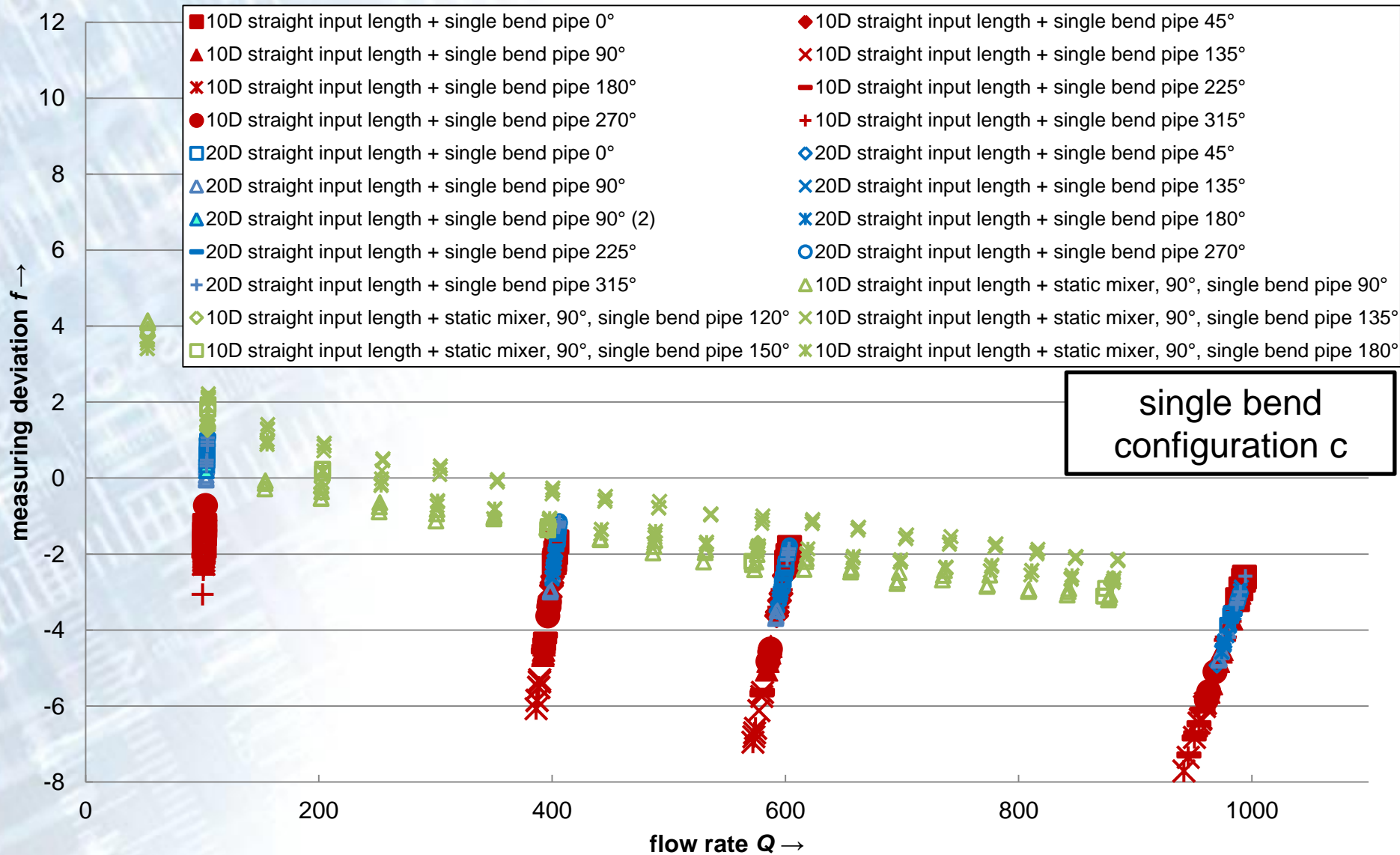
Investigation of the characteristics of the flow metering unit



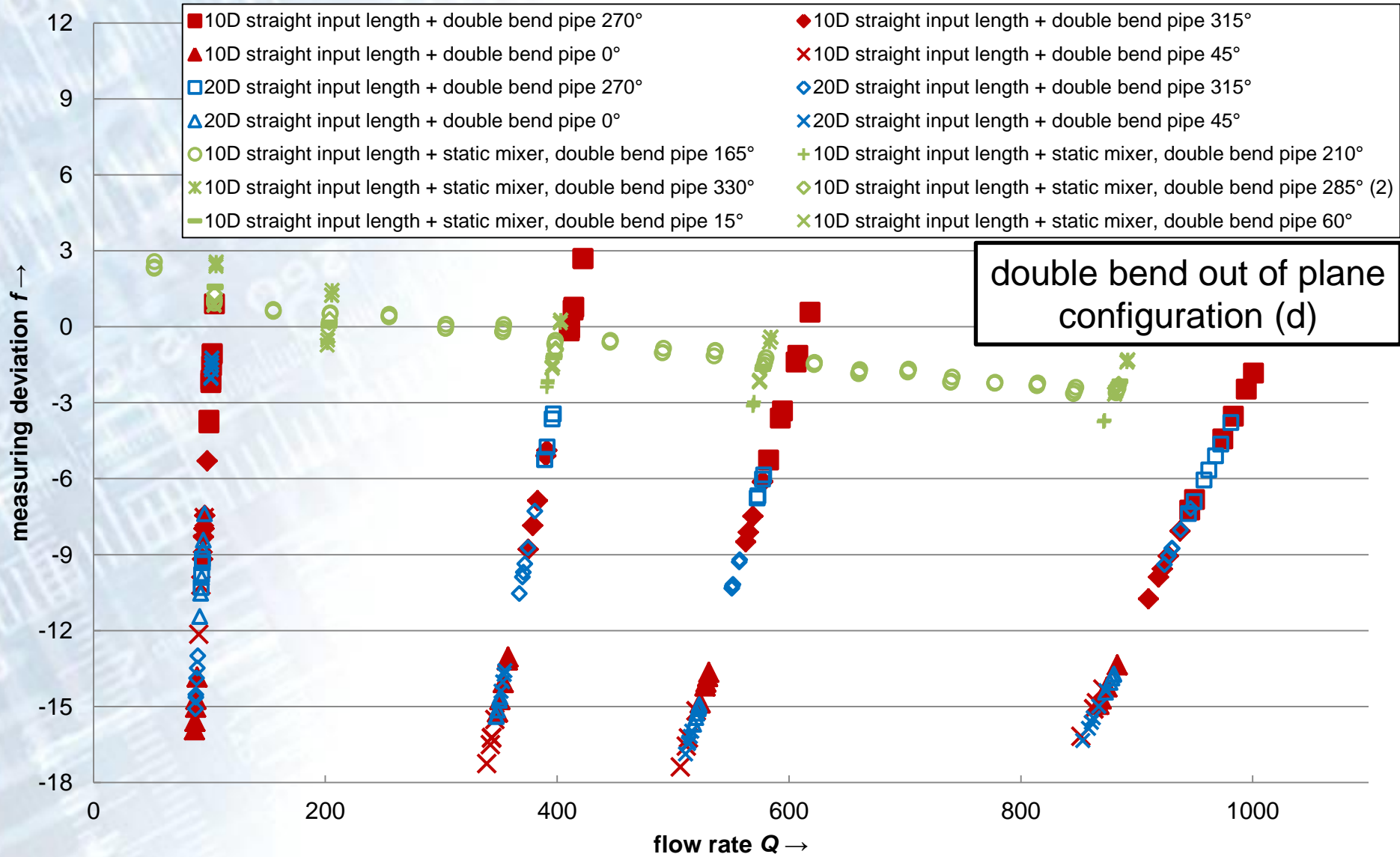
Investigation of the characteristics of the flow metering unit



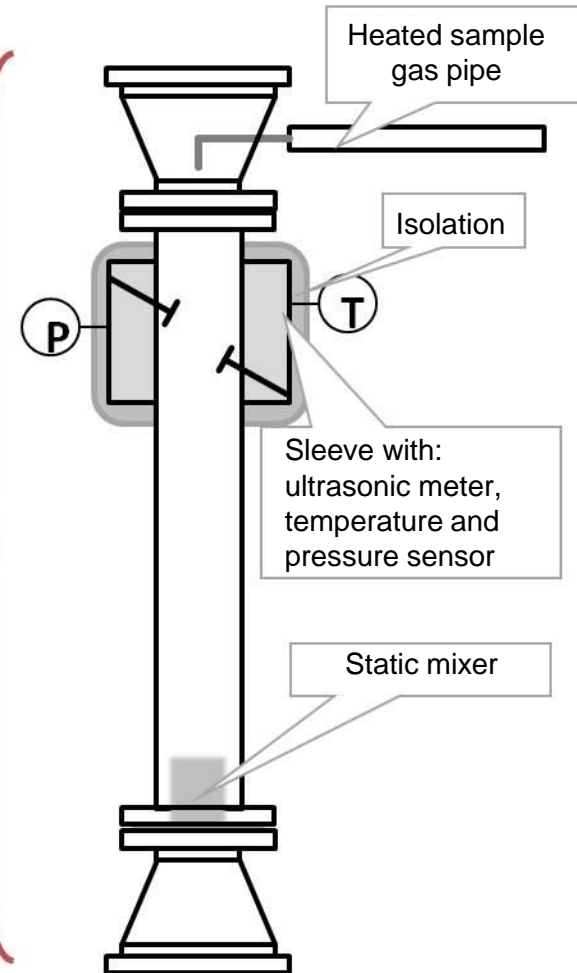
Investigation of the characteristics of the flow metering unit



Investigation of the characteristics of the flow metering unit



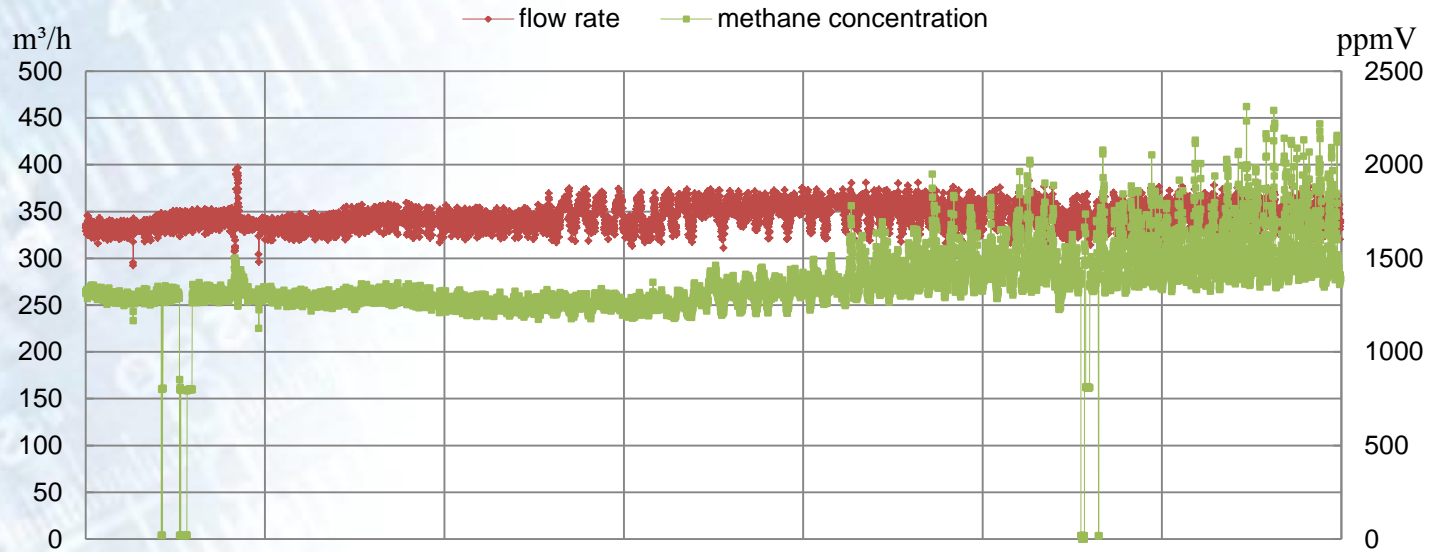
Practical experience



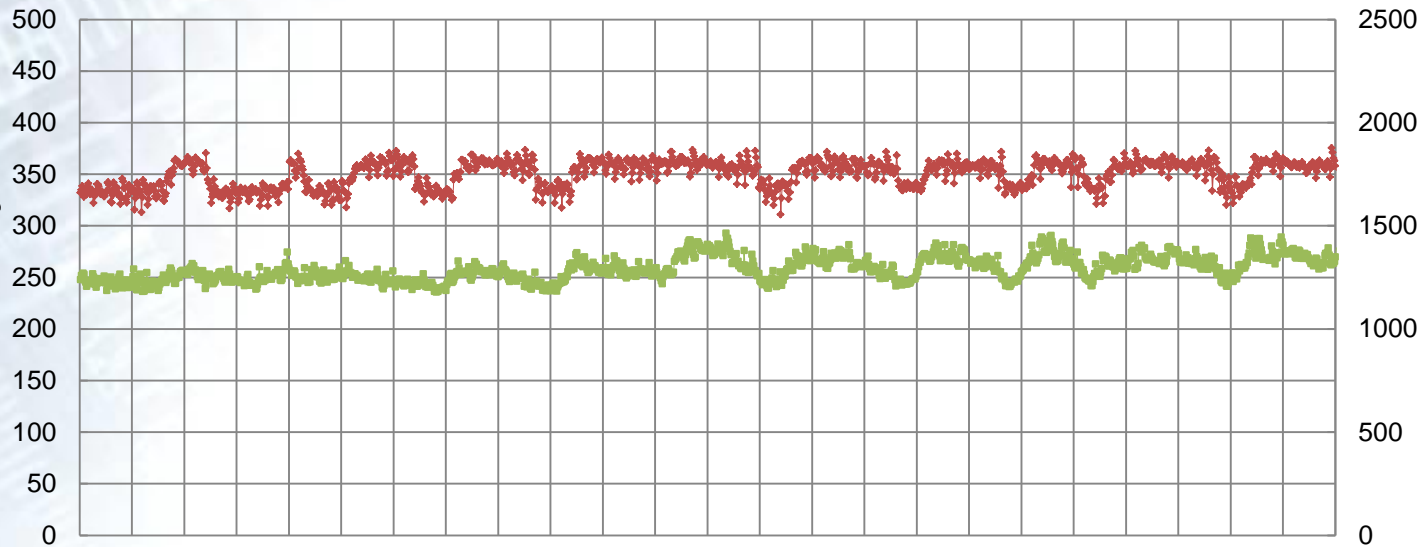
Practical experience

chemical scrubbing (amine scrubbing)

a week

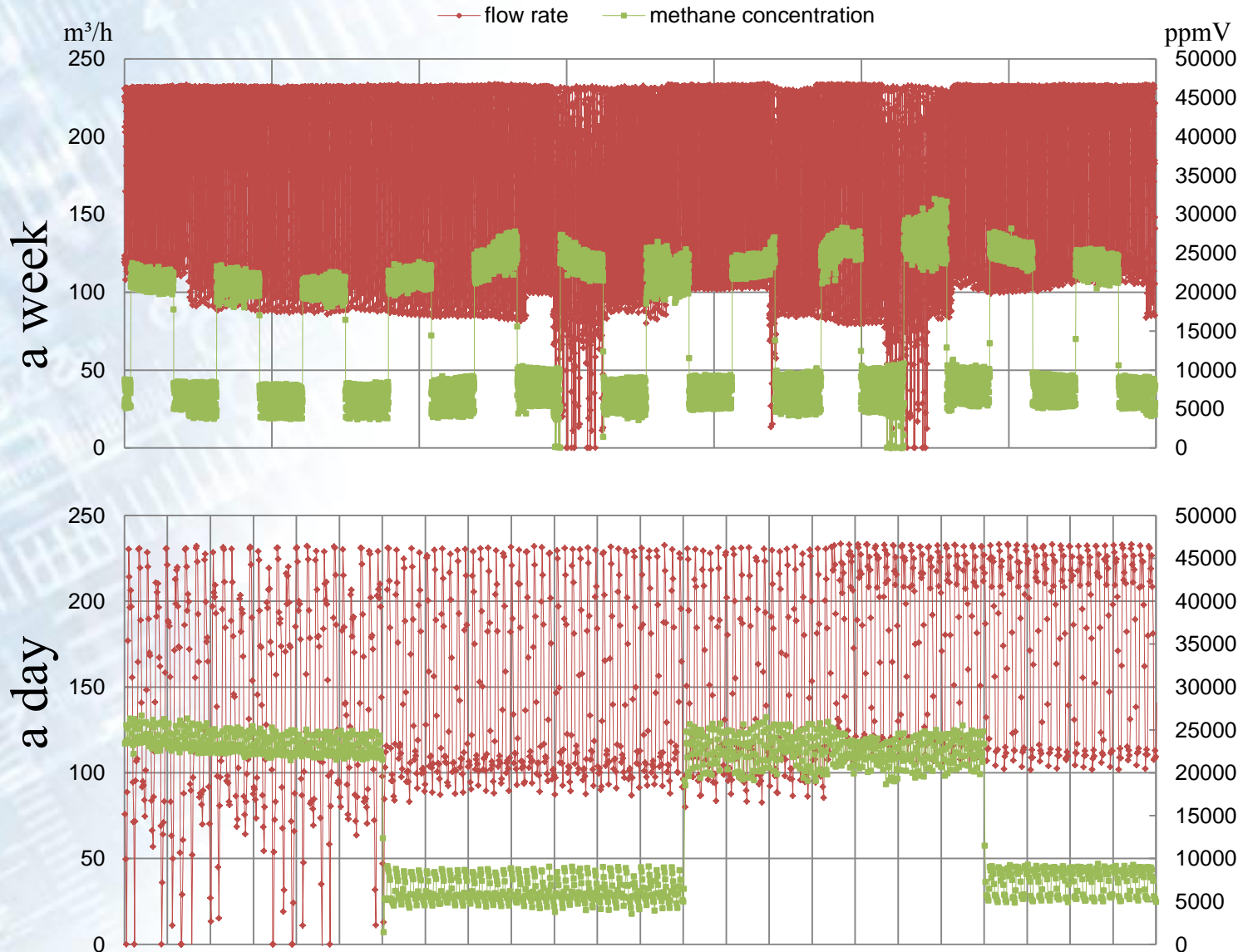


a day



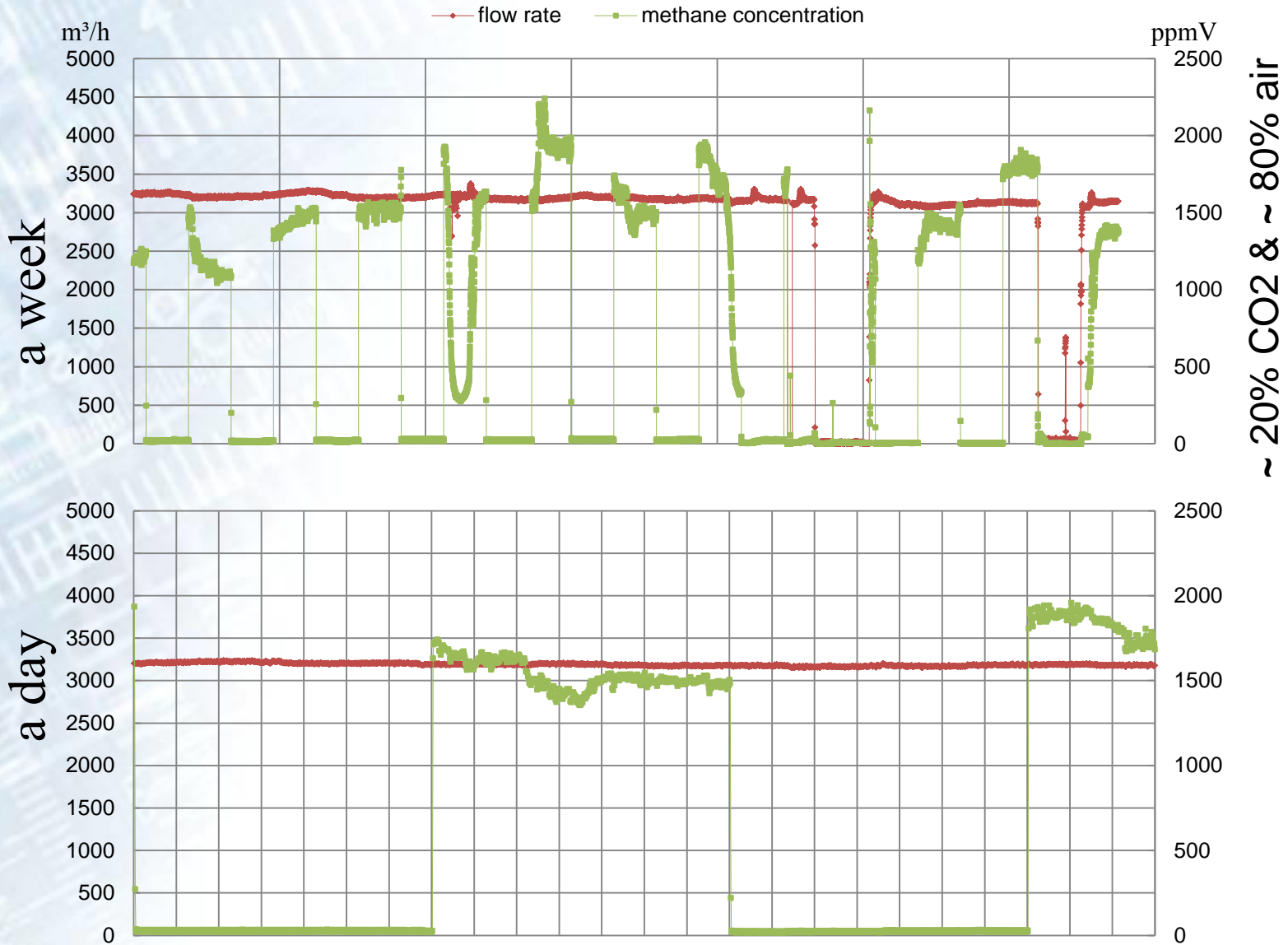
Practical experience

pressure swind adsorbtion



Practical experience

water scrubbing



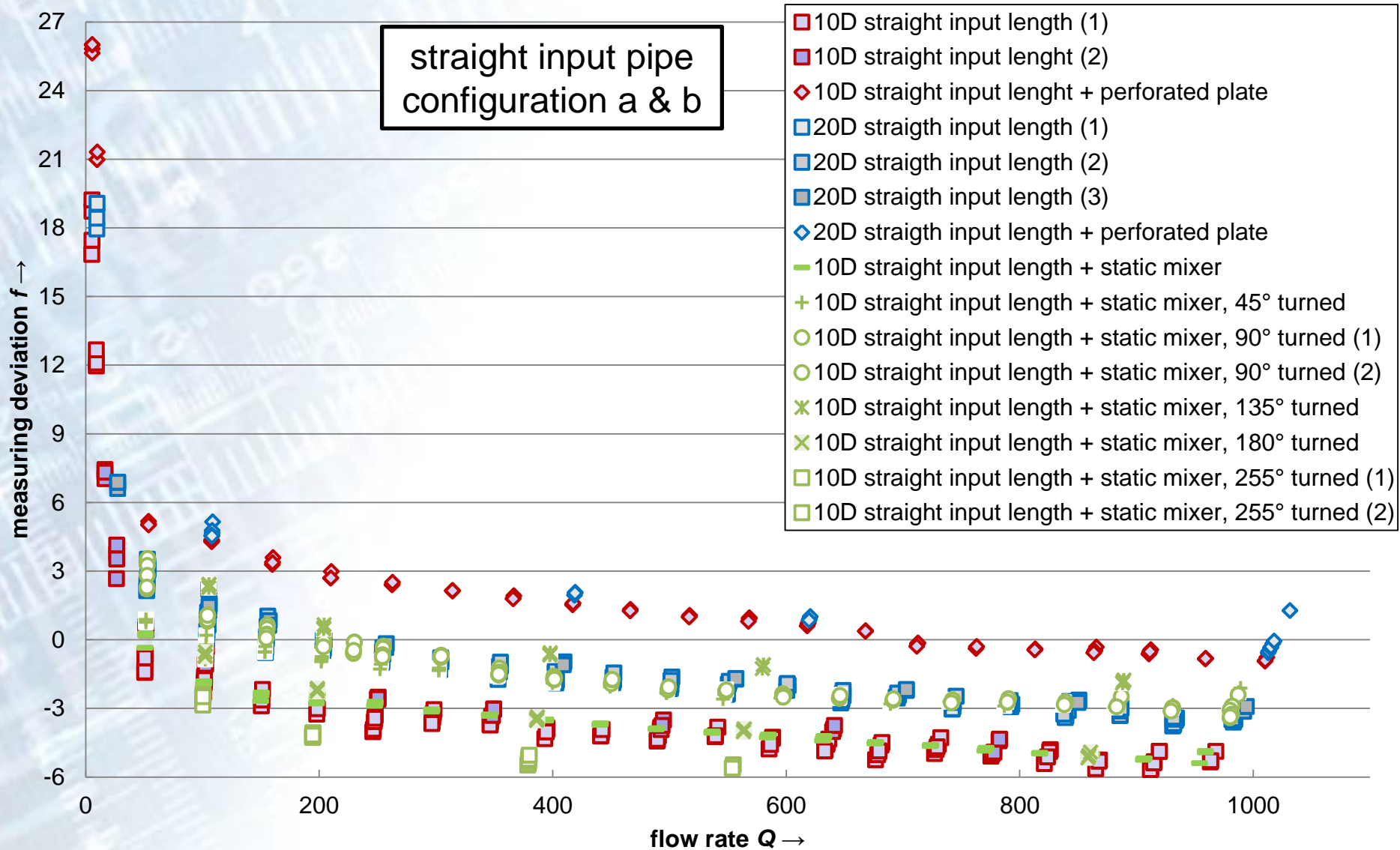
Conclusion

- the mobile measuring system is able to measure to memorise and to transmit data for flow rate and methane concentration with a resolution of 1 minute
- the system is designed to acquire data over a period of 2 weeks
- the system works after installation and putting into use without personnel on site
- an uncertainty of $U = 2\%$ for the volume flow rate determination is reachable if sufficient straight pipe length is given or if the installation of a flow straightener is possible
- the measurement on site show different emission levels, depending on the used upgrading technique
- further focus shall be on the influences of upstream conditions on the meter behavior and the influence of the matrix on the methane concentration

: Time-resolved investigation of the exhaust emissions of upgrading units

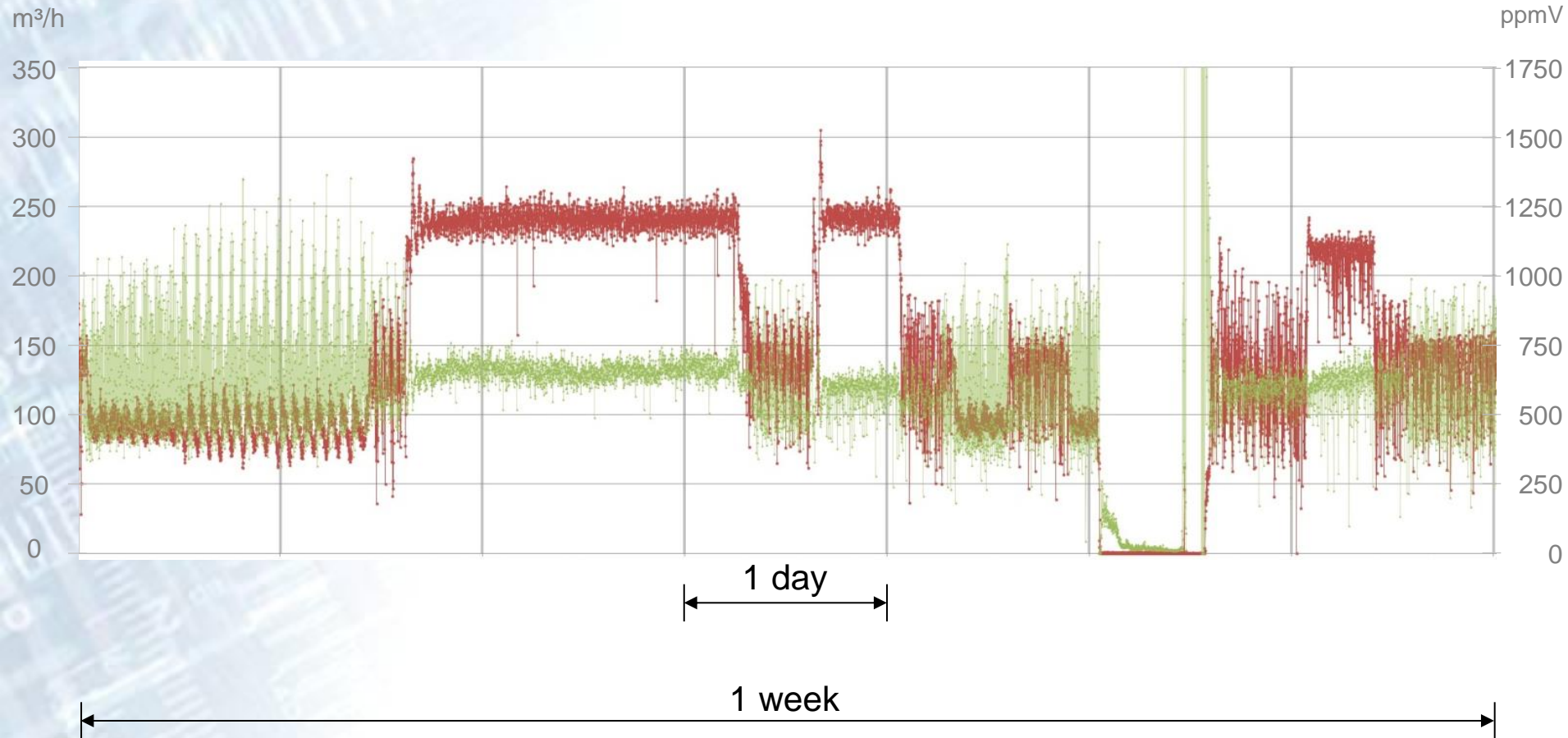


Investigation of the characteristics of the flow metering unit

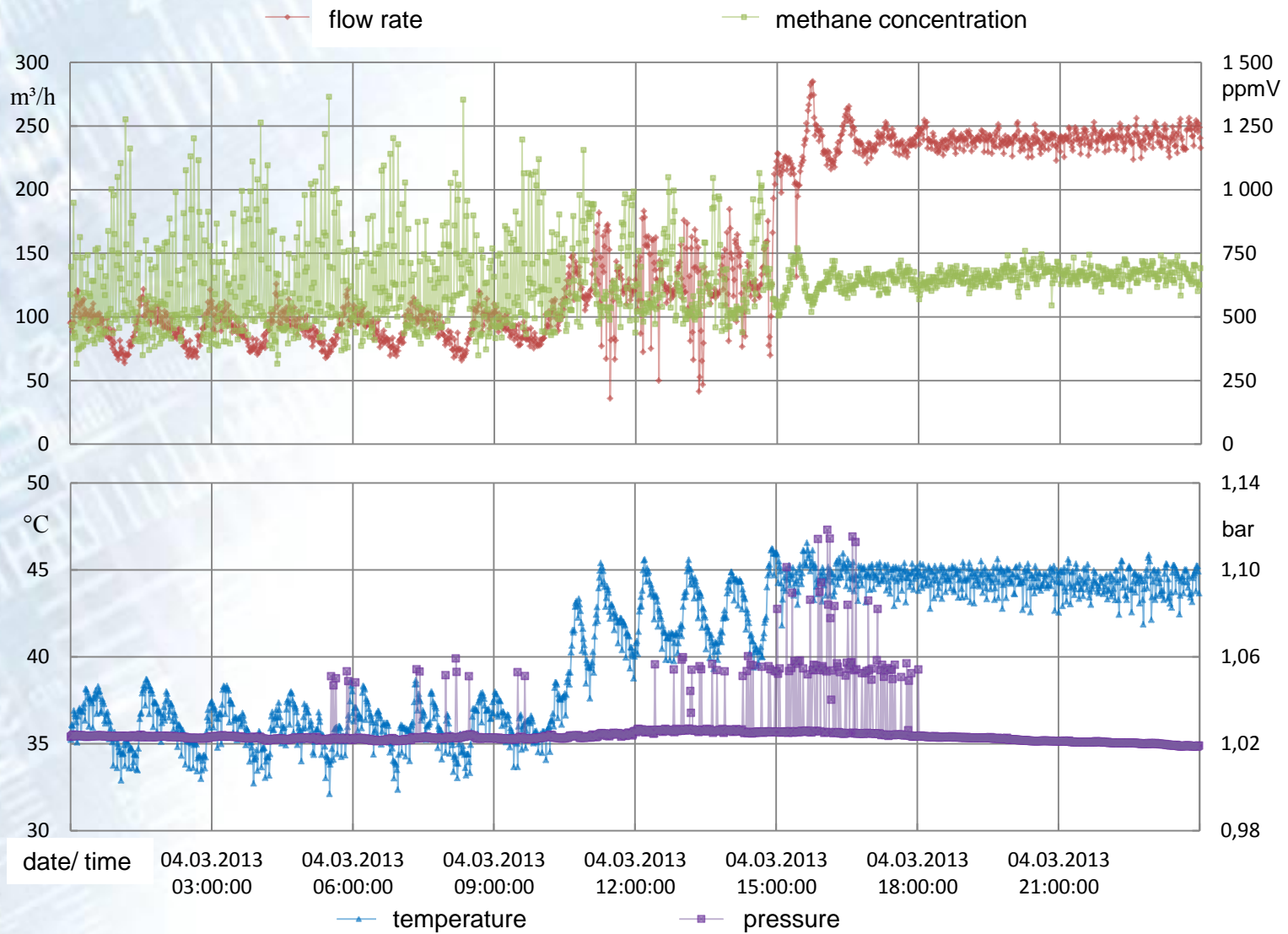


Practical experience

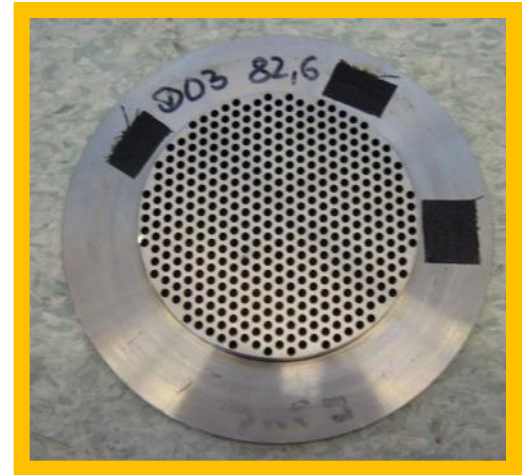
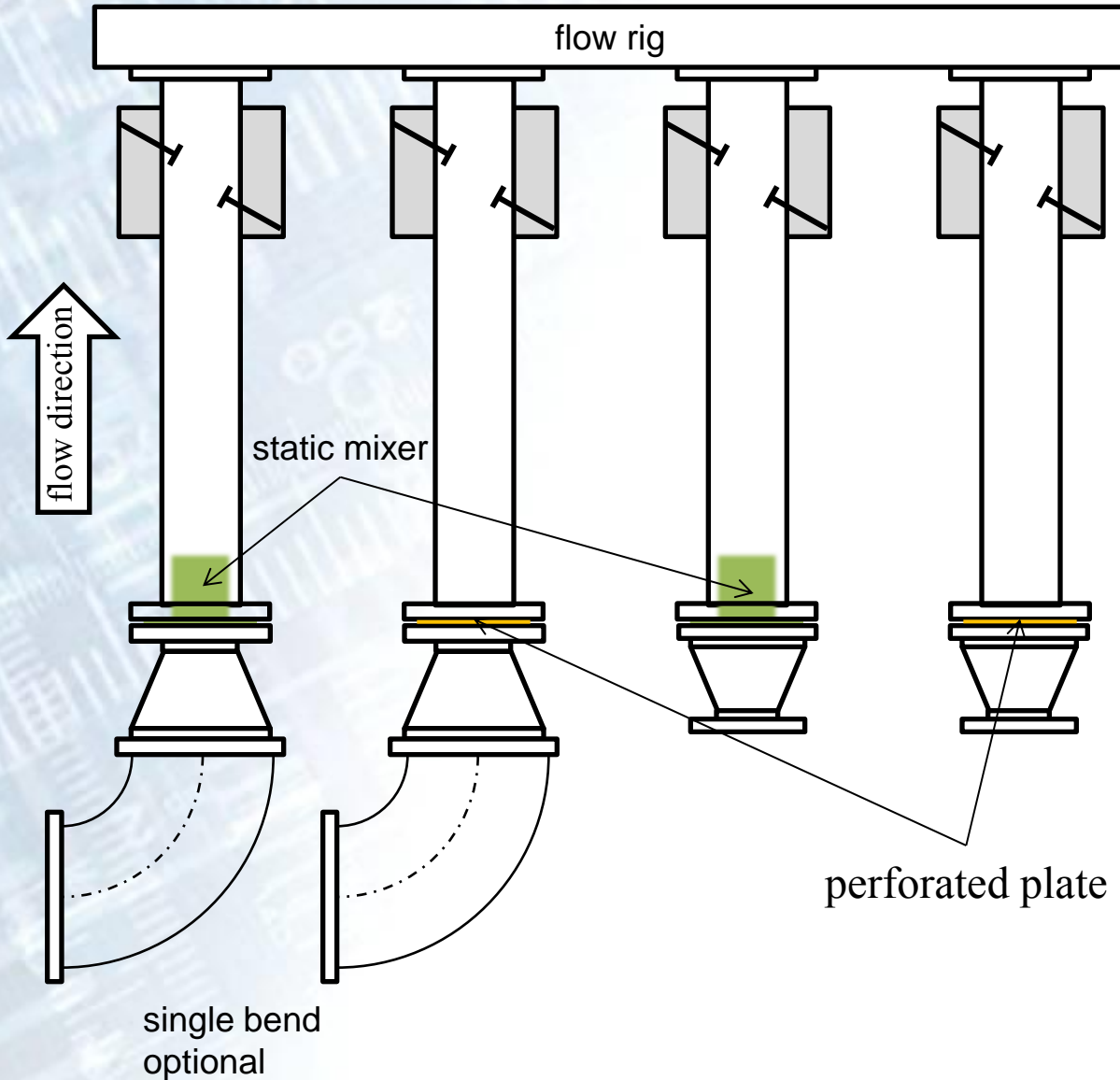
—•— flow rate
 —•— methane concentration



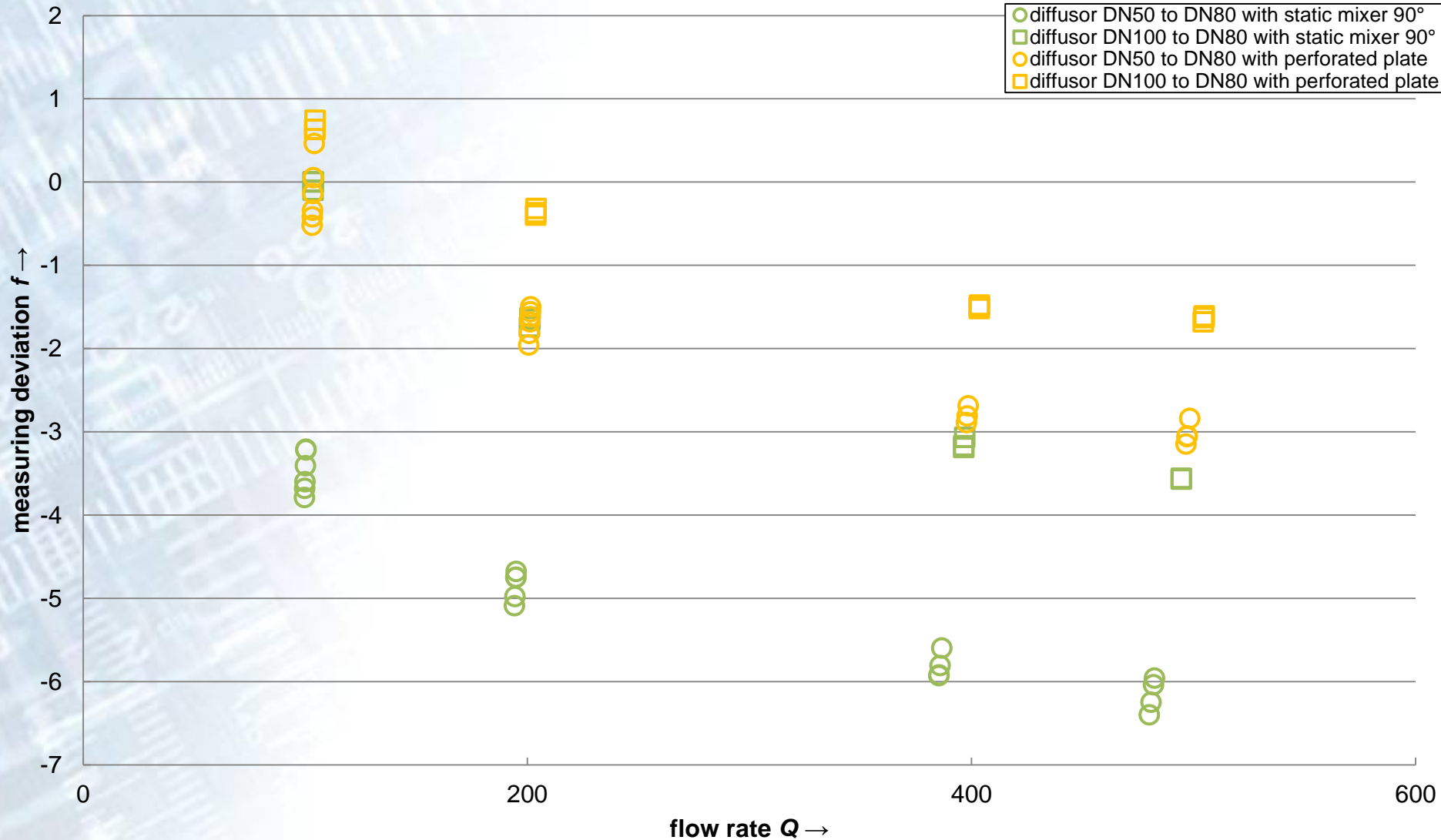
Practical experience



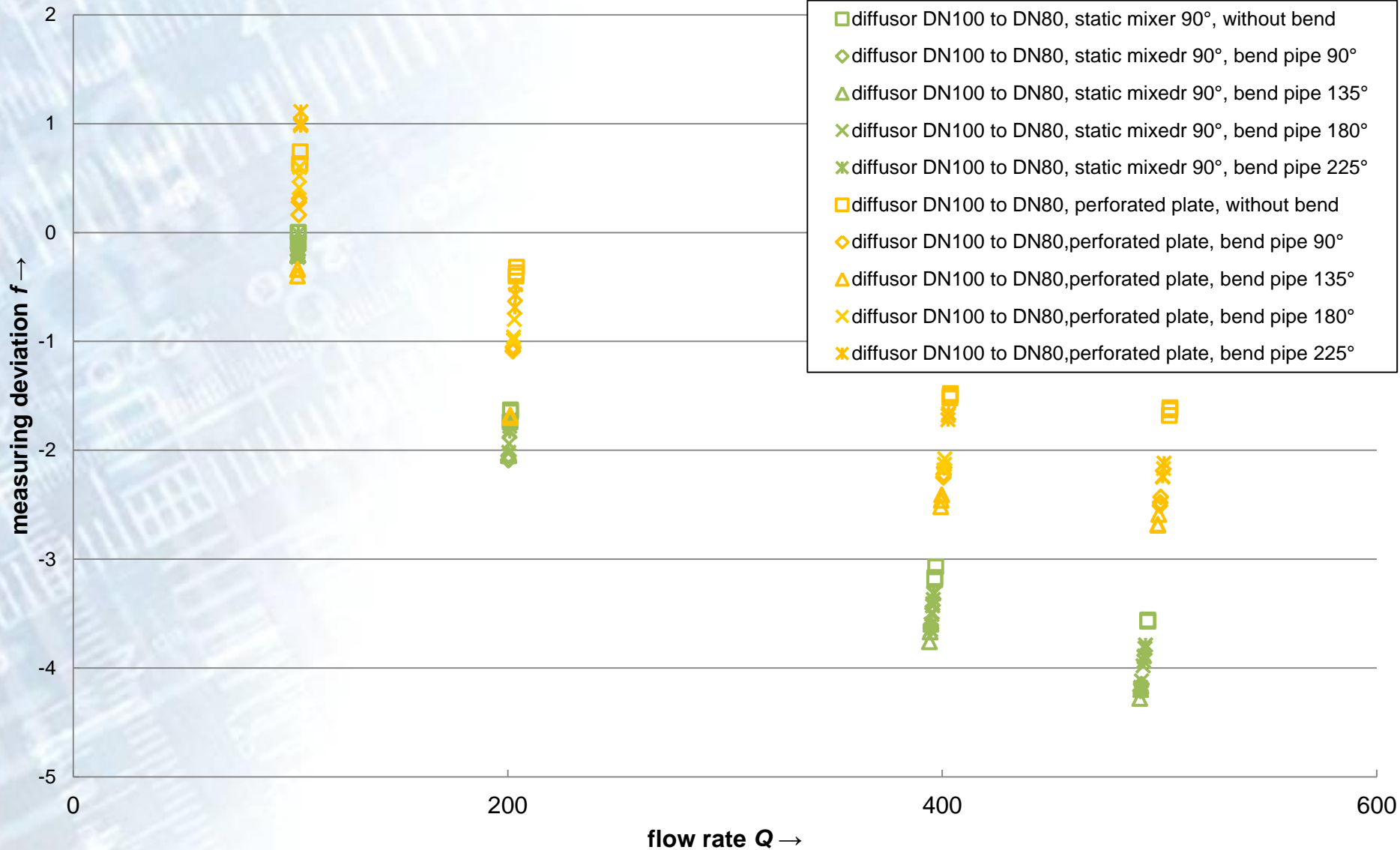
Investigation of the characteristics of the flow metering unit



Investigation of the characteristics of the flow metering unit

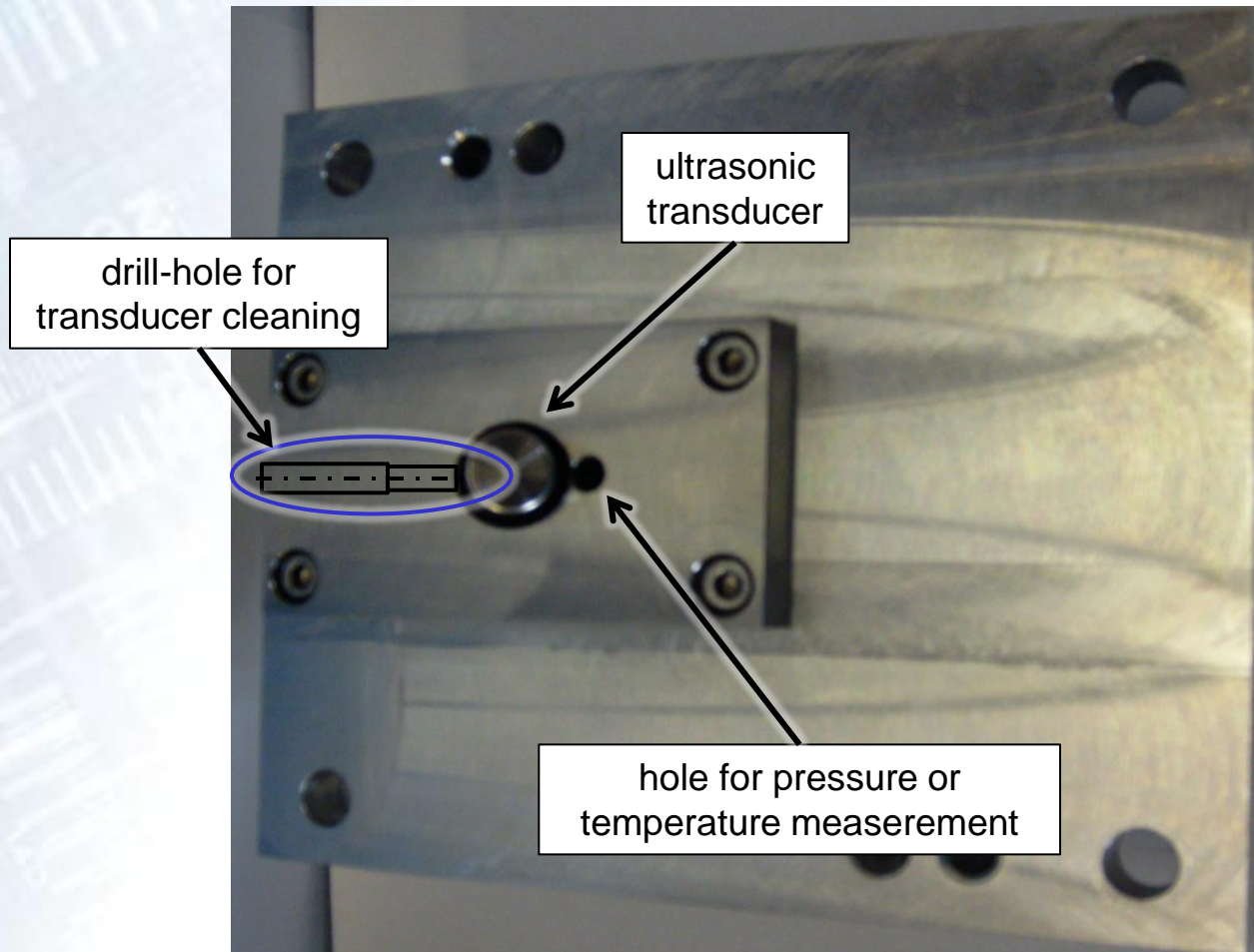


Investigation of the characteristics of the flow metering unit



Practical experience

bottom plate of the sleeve



Measuring equipment

Verfahren	Vorteile	Nachteile
kommerziell verfügbare Zähler	<ul style="list-style-type: none"> hohe Messgenauigkeit geringe Vorstörungsempfindlichkeit (typabhängig) 	<ul style="list-style-type: none"> keine Flansche vorhanden starker Eingriff in die Anlagenstruktur hoher Einbauaufwand
Ultraschalllanze	<ul style="list-style-type: none"> geringer Eingriff in die Anlagenstruktur (nur eine Bohrung erforderlich) 	<ul style="list-style-type: none"> nur Ausschnitte des Profils messbar Winkeljustage schwierig wegen der Größe der Sensoren in Rohren <DN100 nur bedingt brauchbar
Ultraschallmessung als Clamp-On-Technik	<ul style="list-style-type: none"> kein Eingriff in die Anlagenstruktur 	<ul style="list-style-type: none"> Gasdruck muss ausreichend hoch sein Schalldämpfung von CO₂ kann problematisch sein Temperatur- und Druckmessungen sind nicht möglich Innendurchmesser des Rohrs kann nicht direkt gemessen werden
Einpfad-Ultraschallmessung mit Manschette	<ul style="list-style-type: none"> geringer Eingriff in die Anlagenstruktur (2 Bohrungen) Sensoren können in verschiedenen Manschettengrößen eingesetzt werden 	<ul style="list-style-type: none"> Starke Vorstörungsempfindlichkeit
Wirkdruckmessung (mit Prandtl-Sonde)	<ul style="list-style-type: none"> geringer Eingriff in die Anlagenstruktur (nur eine Bohrung erforderlich) 	<ul style="list-style-type: none"> Sehr starke Vorstörungsempfindlichkeit